

Geometrical Spreading Determined from Coda-Normalized S-wave Amplitudes

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of the National Seismic Hazard Maps
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Describing the Distance Decay of S-wave Spectral Amplitudes at less than 70 km distance

- S-wave Fourier spectral amplitude proportional to:

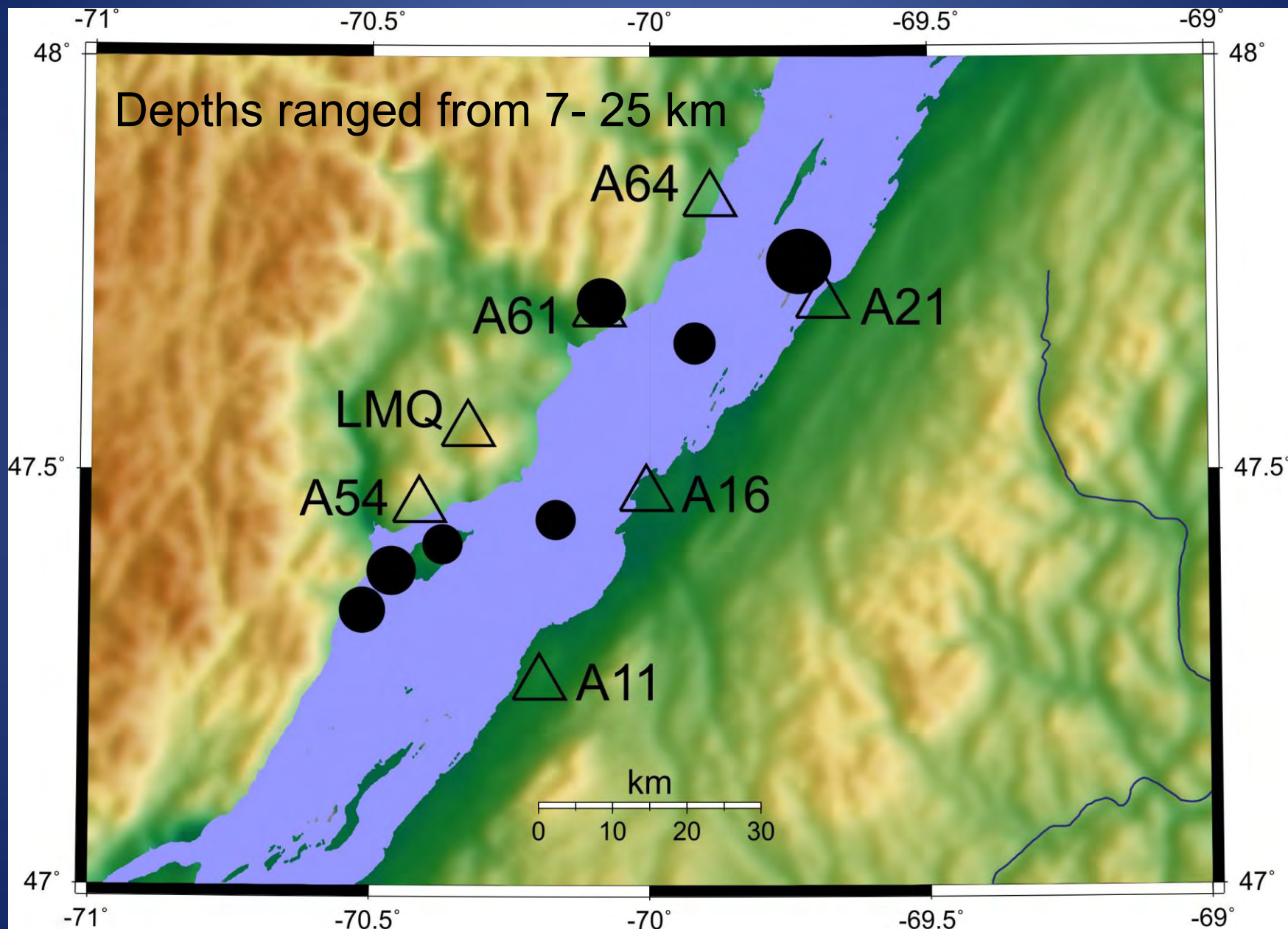
$$S(f)G(f) R^{-\gamma} e^{-\pi ft/Q(f)}$$

$S(f)$ = source spectrum

$G(f)$ = site amplification

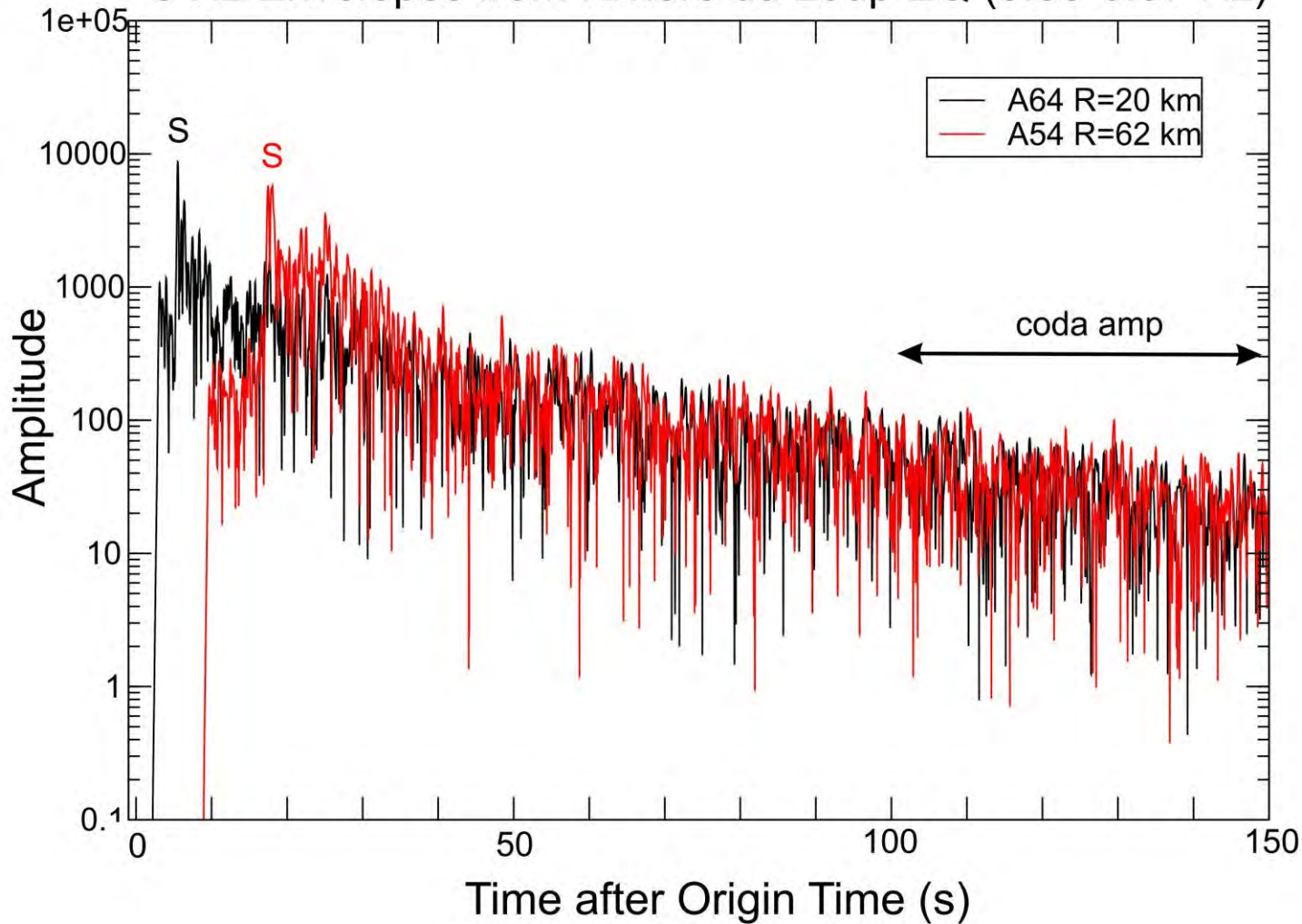
- Used 7 earthquakes in Charlevoix area to study geometrical spreading at distances less than 70 km; data from the Canadian seismic network
- Used horizontal broadband records, except when clipped, then used accelerometer records
- Applied coda normalization technique (Aki, 1982): divide S-wave spectral amplitude by coda amplitude at fixed time after origin time of earthquake to remove site response and source term.

M_n of earthquakes studied ranged from 3.3 to 5.4 (locations and M_n from GSC)

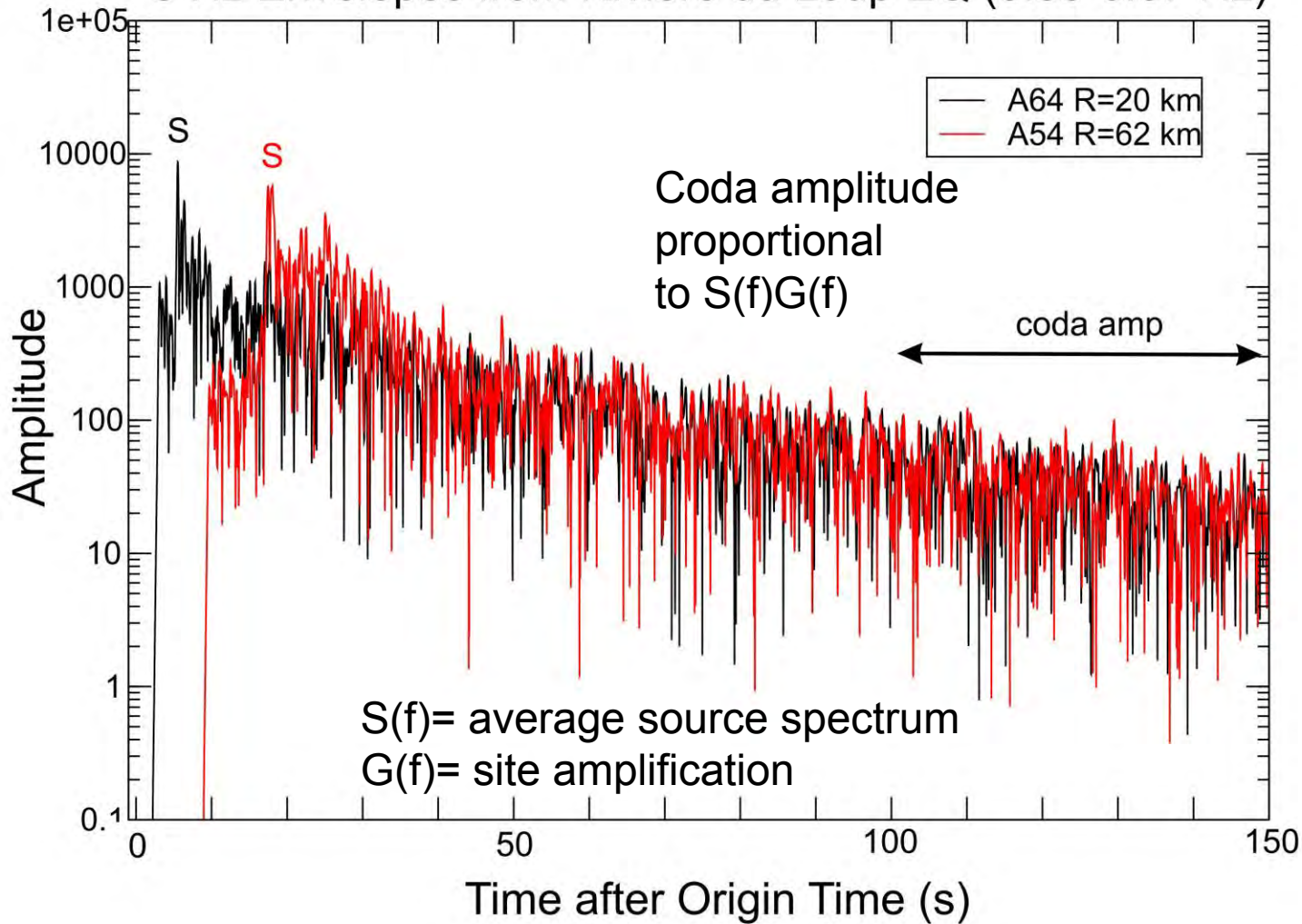


Stations from the Canadian Seismic Network

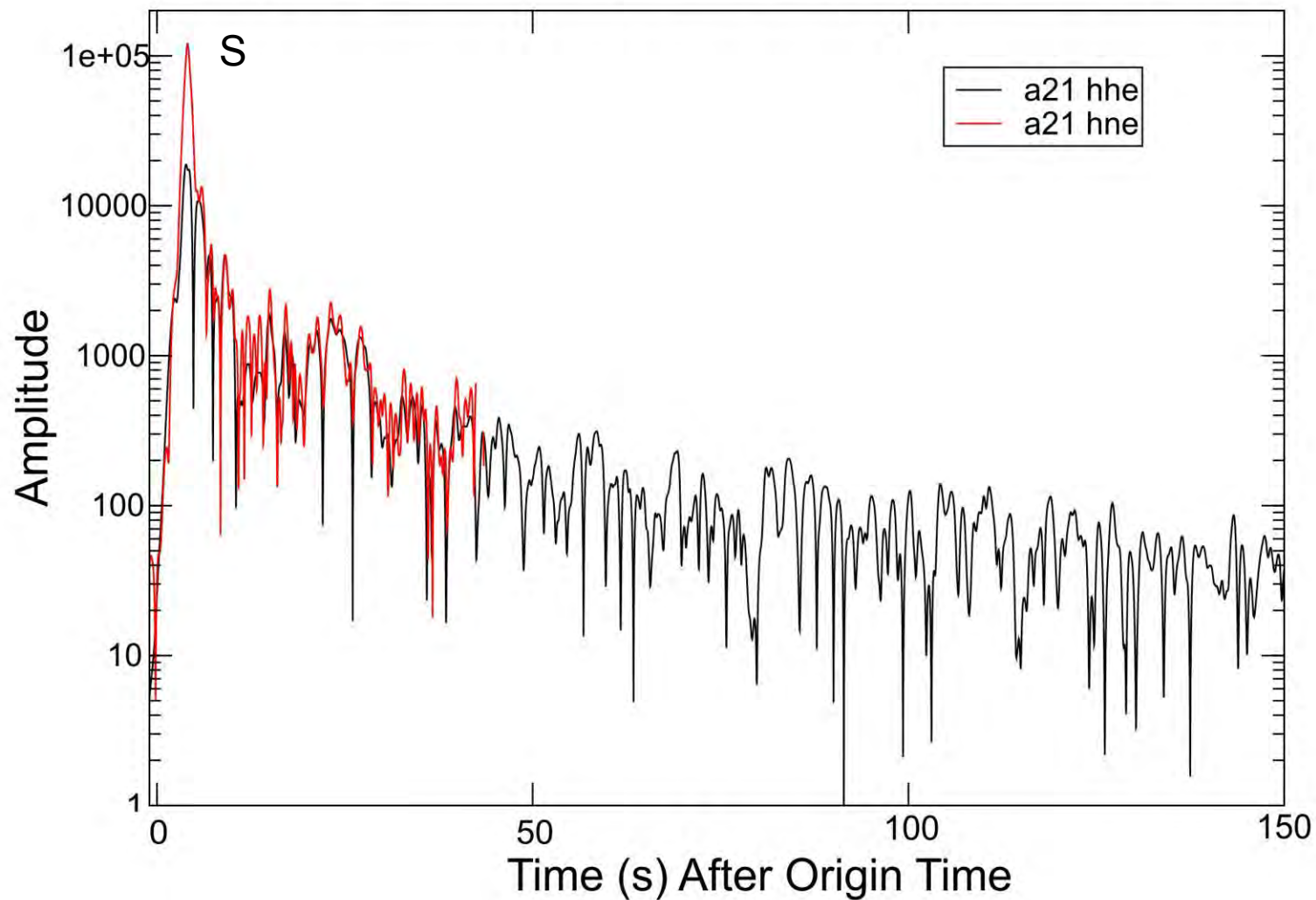
5 Hz Envelopes from Riviere du Loup EQ (3.33-6.67 Hz)



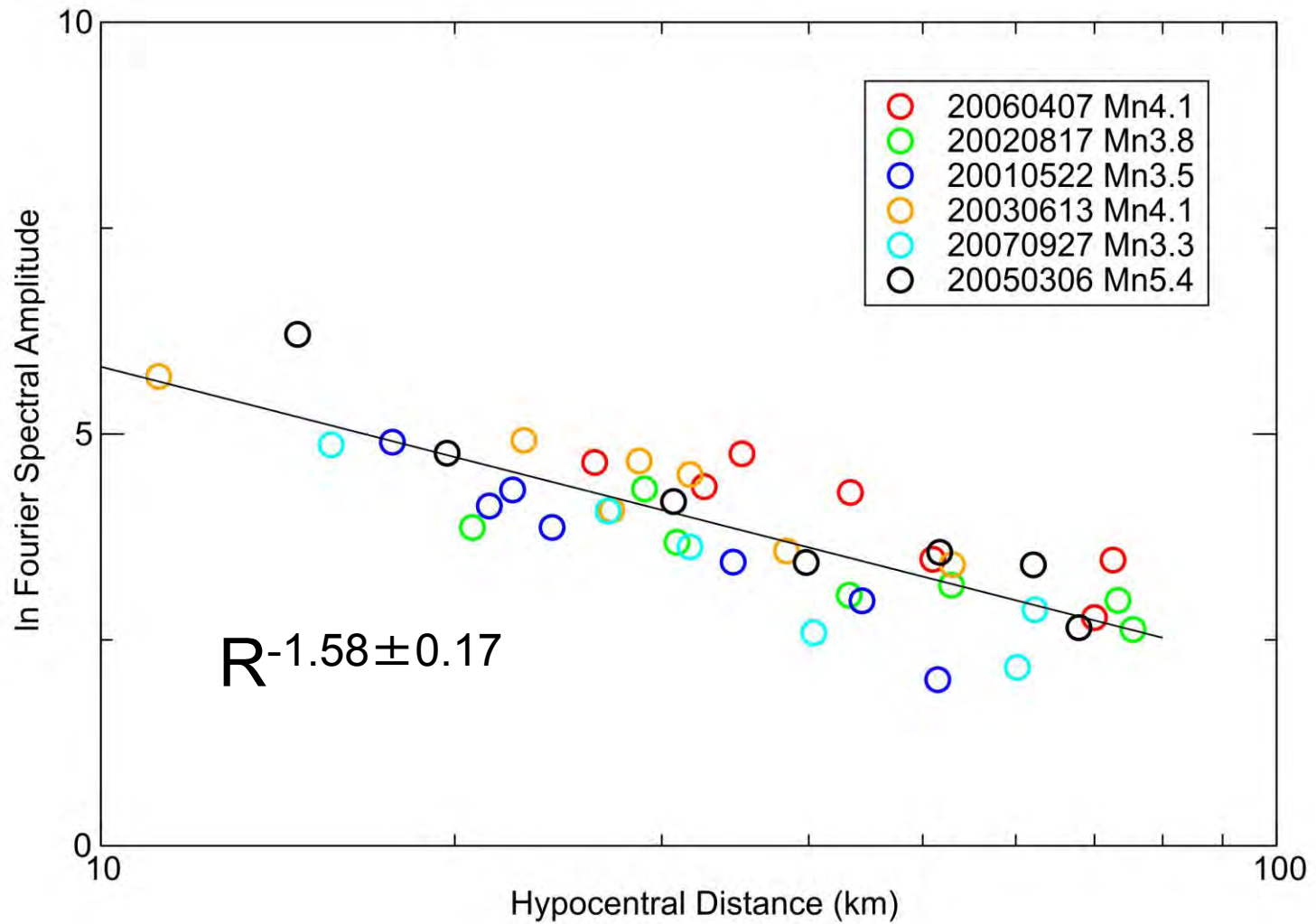
5 Hz Envelopes from Riviere du Loup EQ (3.33-6.67 Hz)



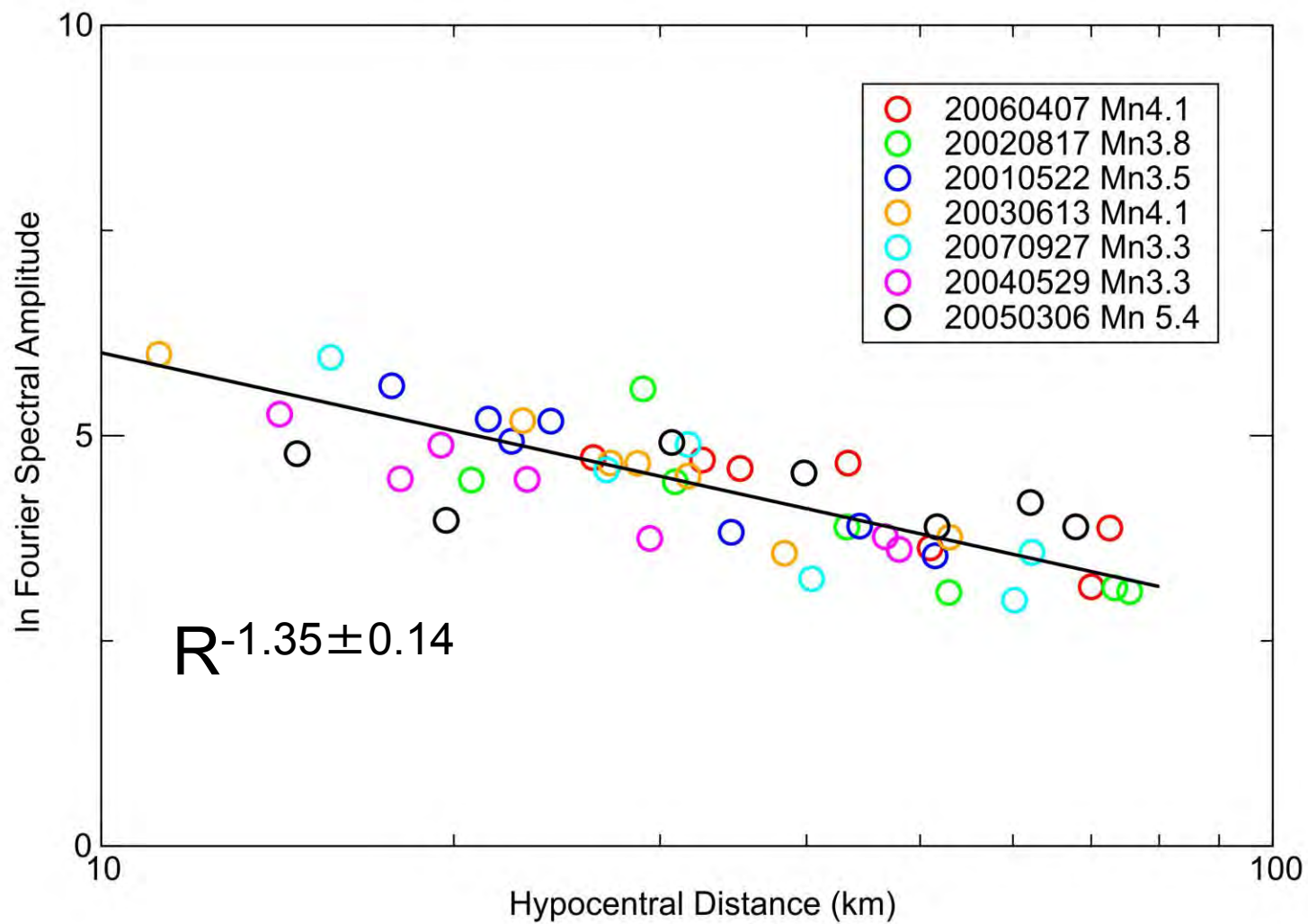
Envelopes of Band-Pass Filtered Seismograms 0.67-1.33 Hz



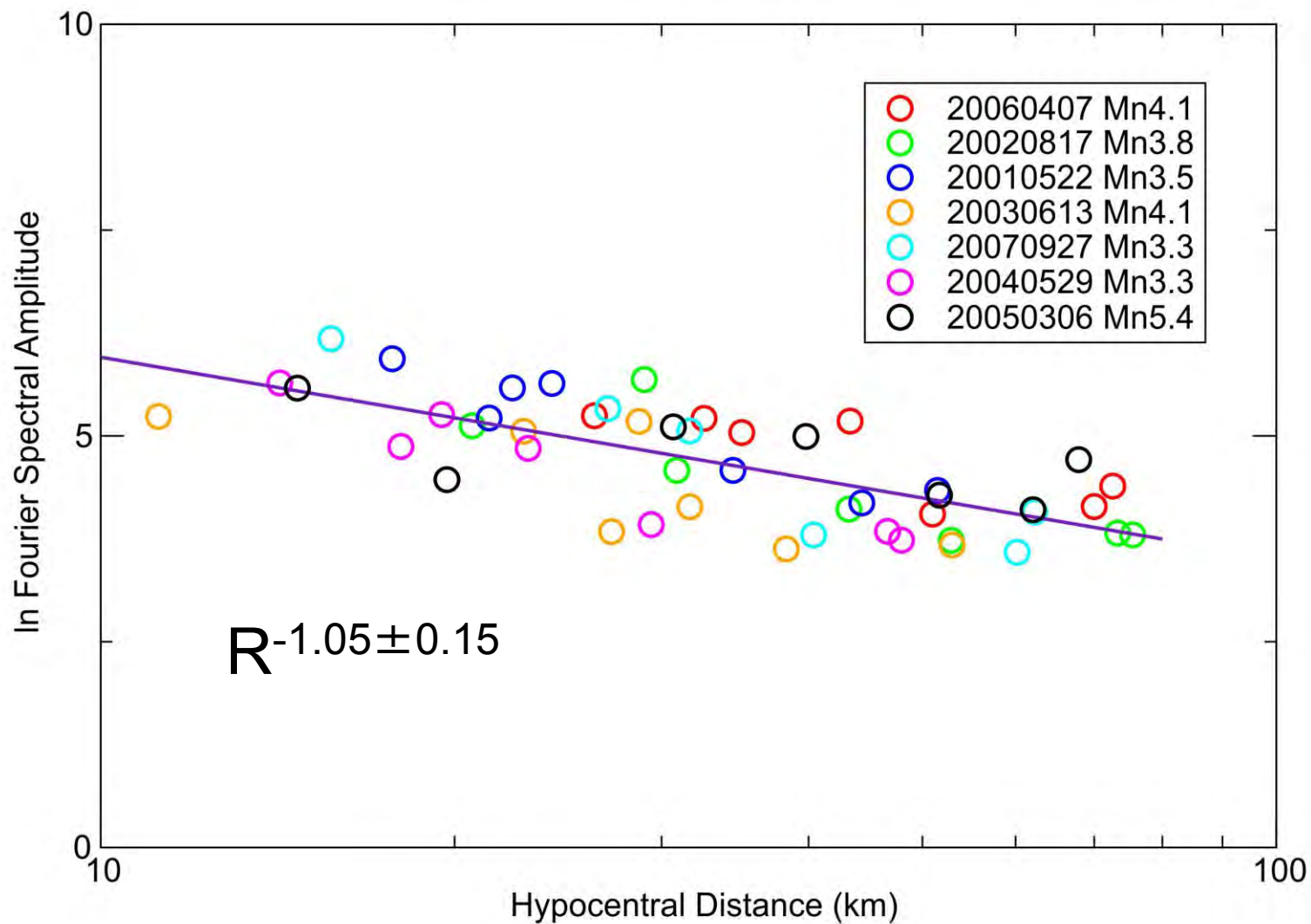
1 Hz



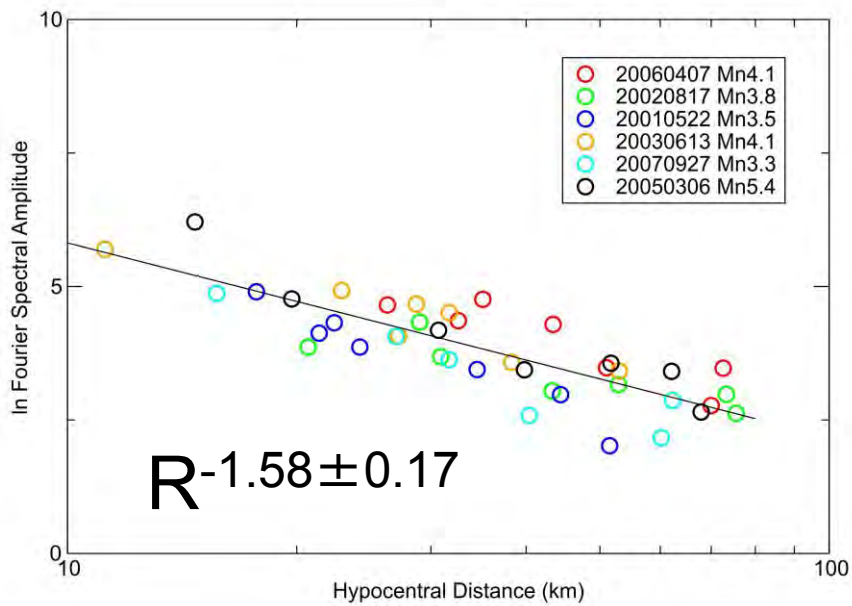
5 Hz



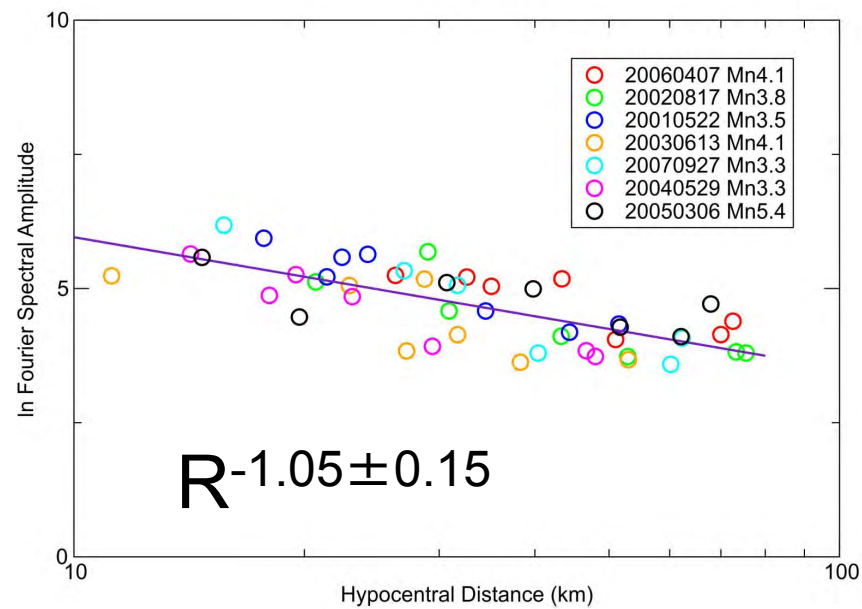
14 Hz



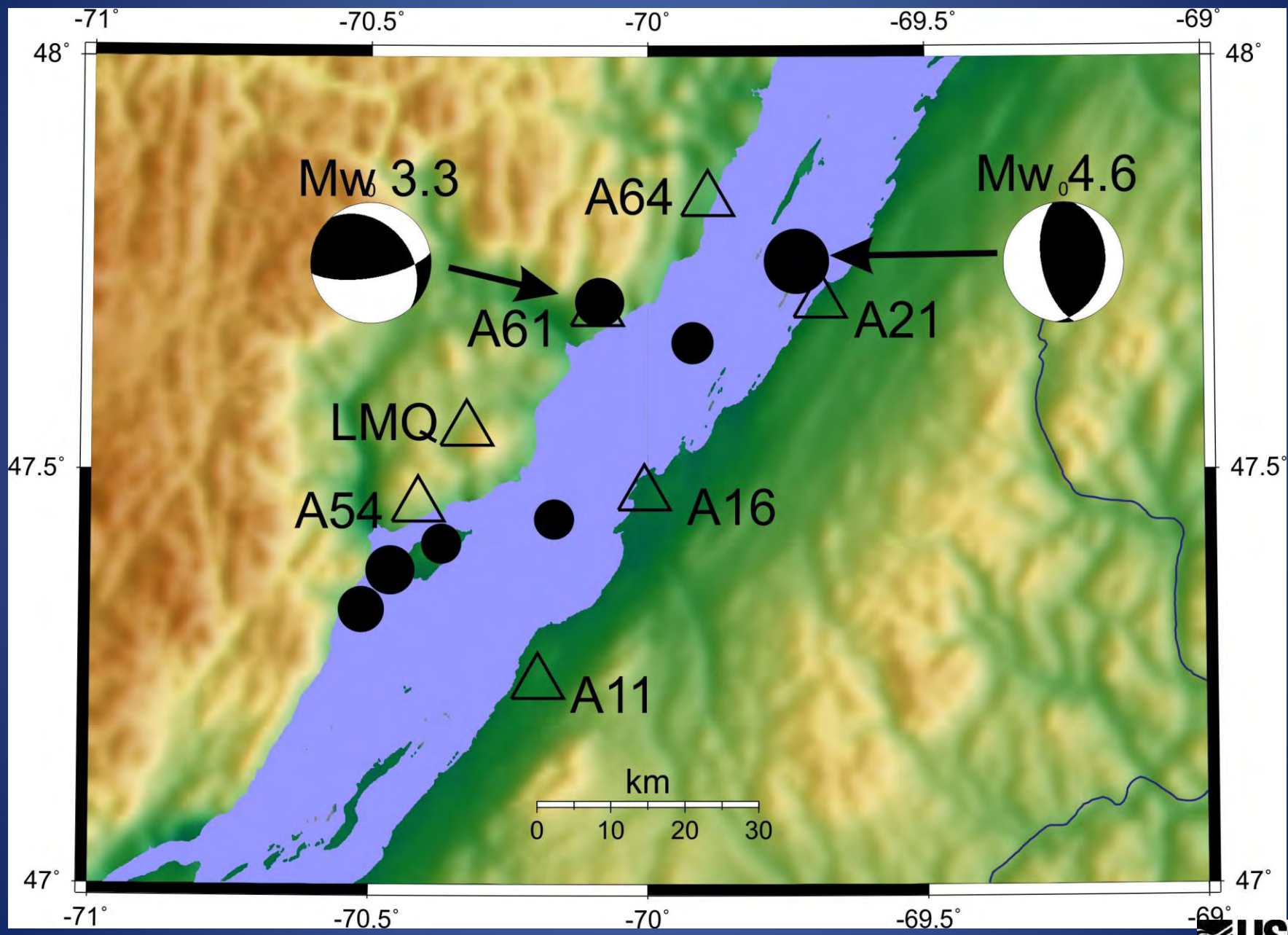
1 Hz



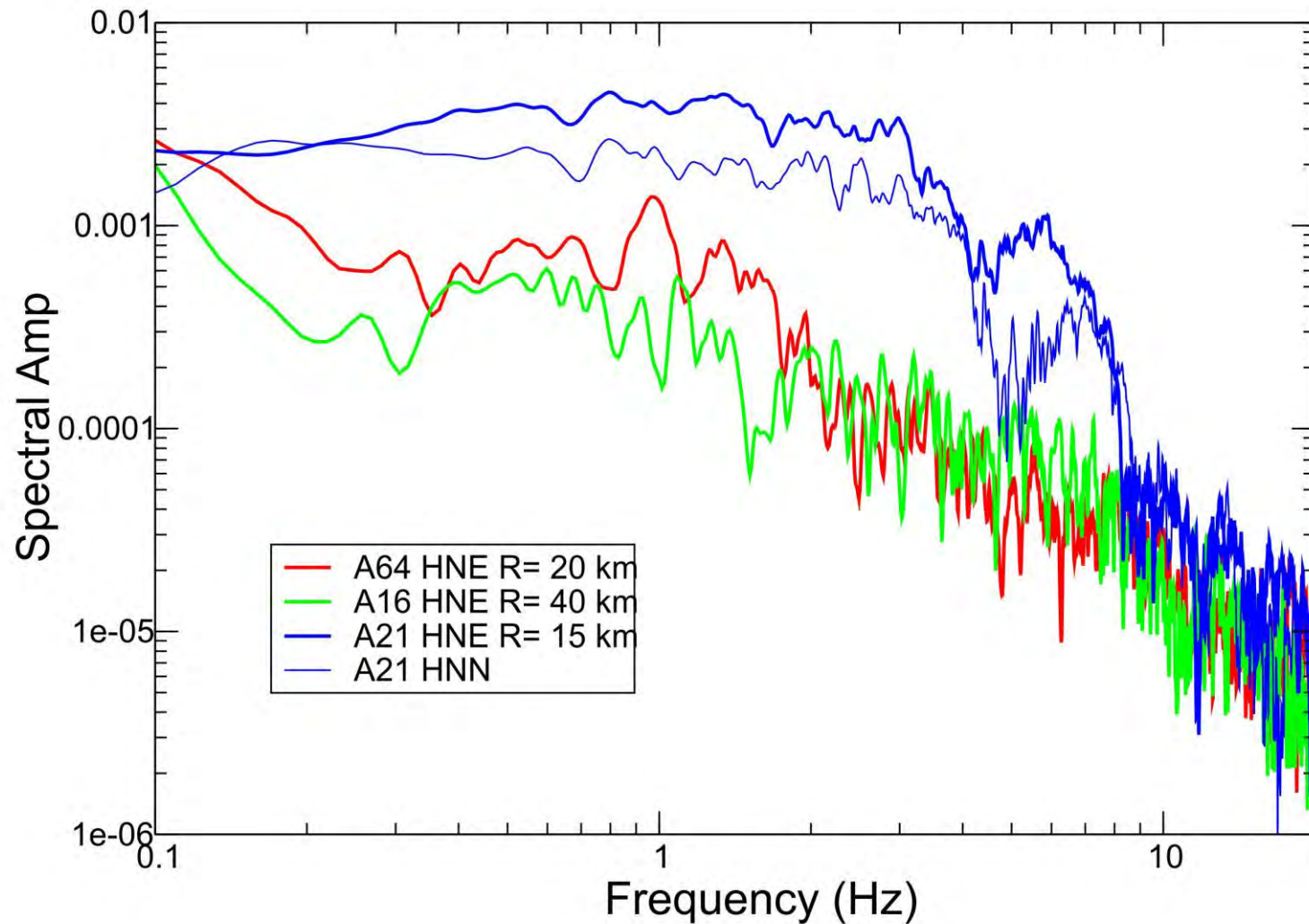
14 Hz



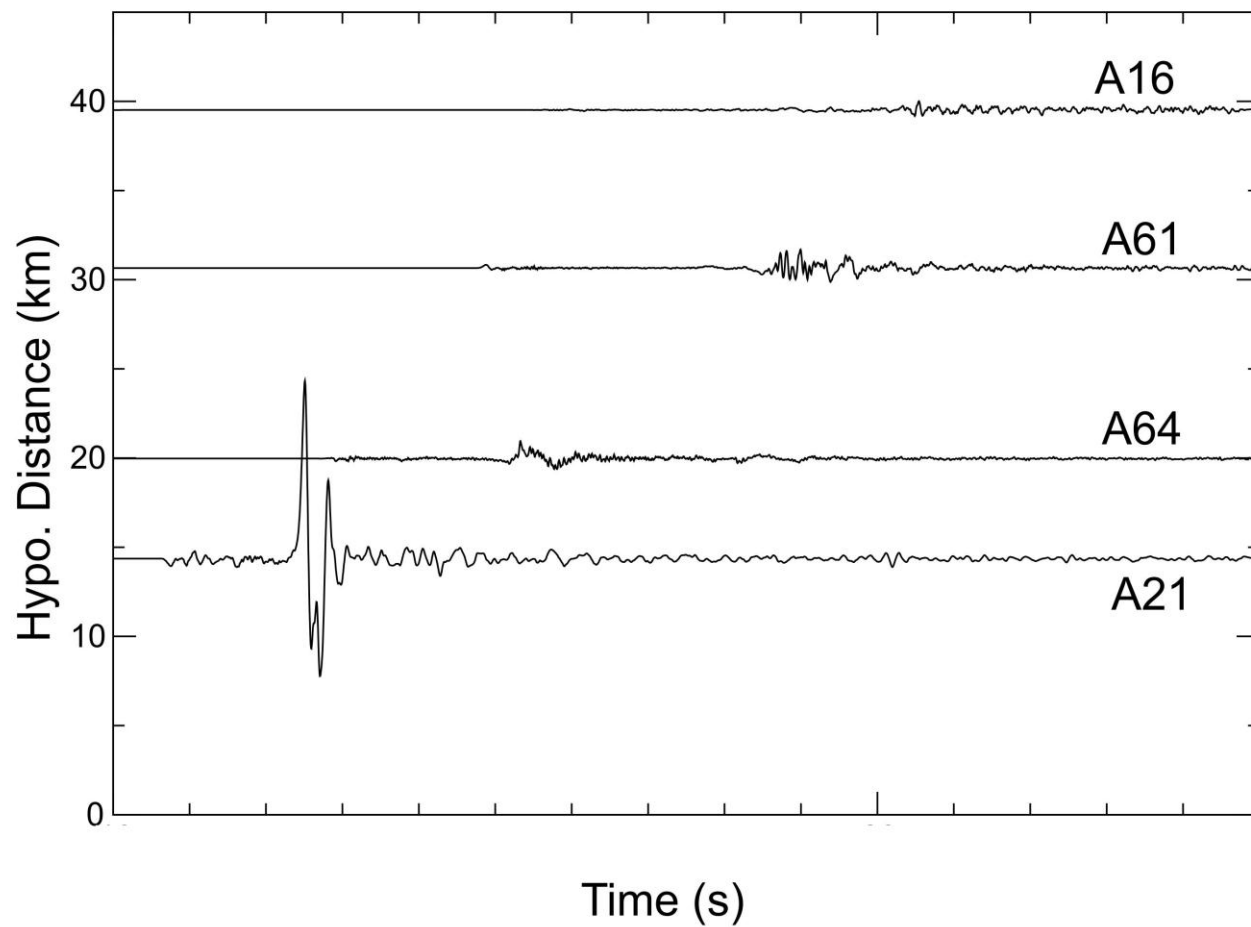
Investigate role of radiation pattern and rupture directivity on distance decay of 1 Hz amp



Riviere du Loup Displacement Spectra



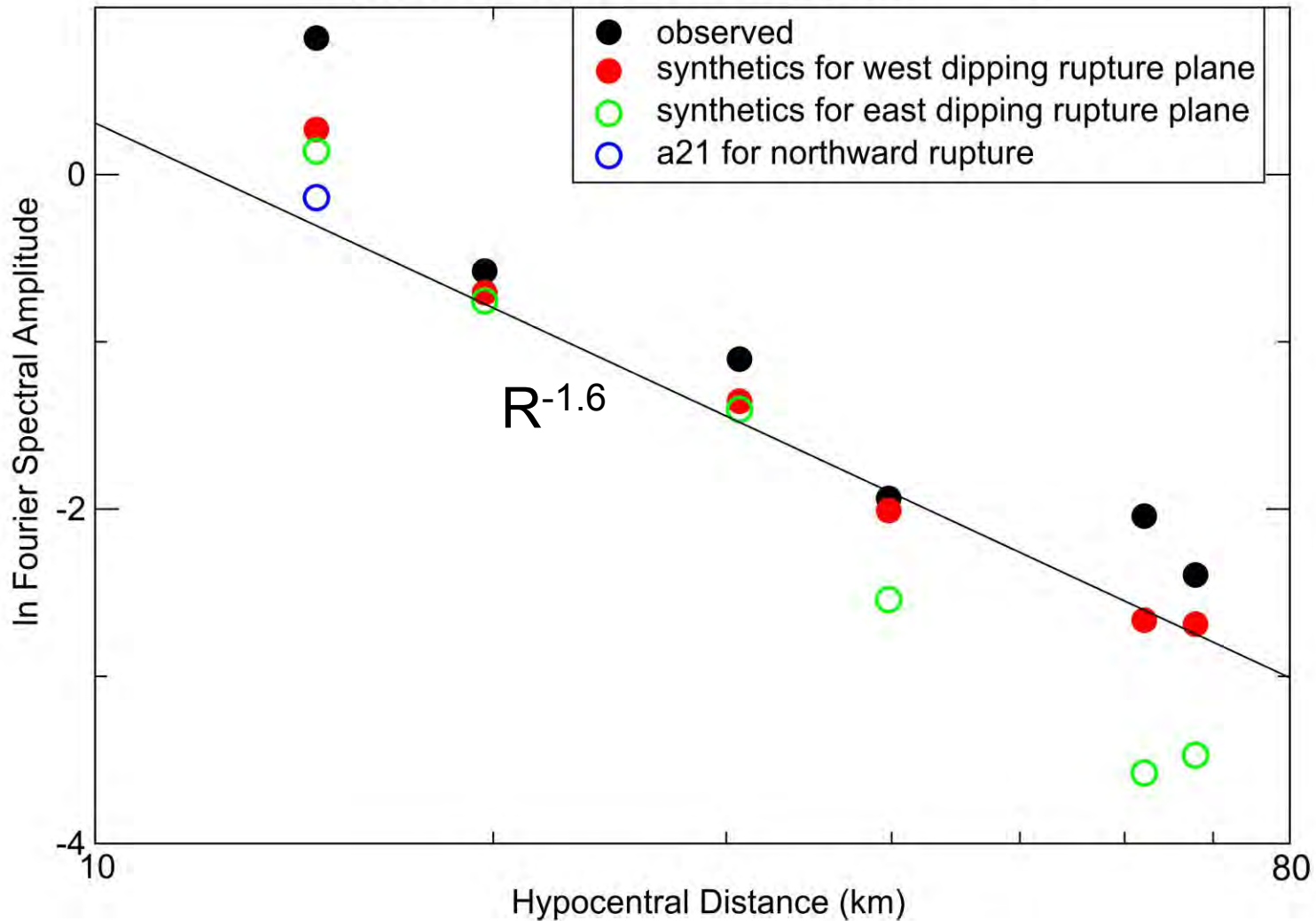
Radial Velocity Waveforms for Riviere du Loup EQ



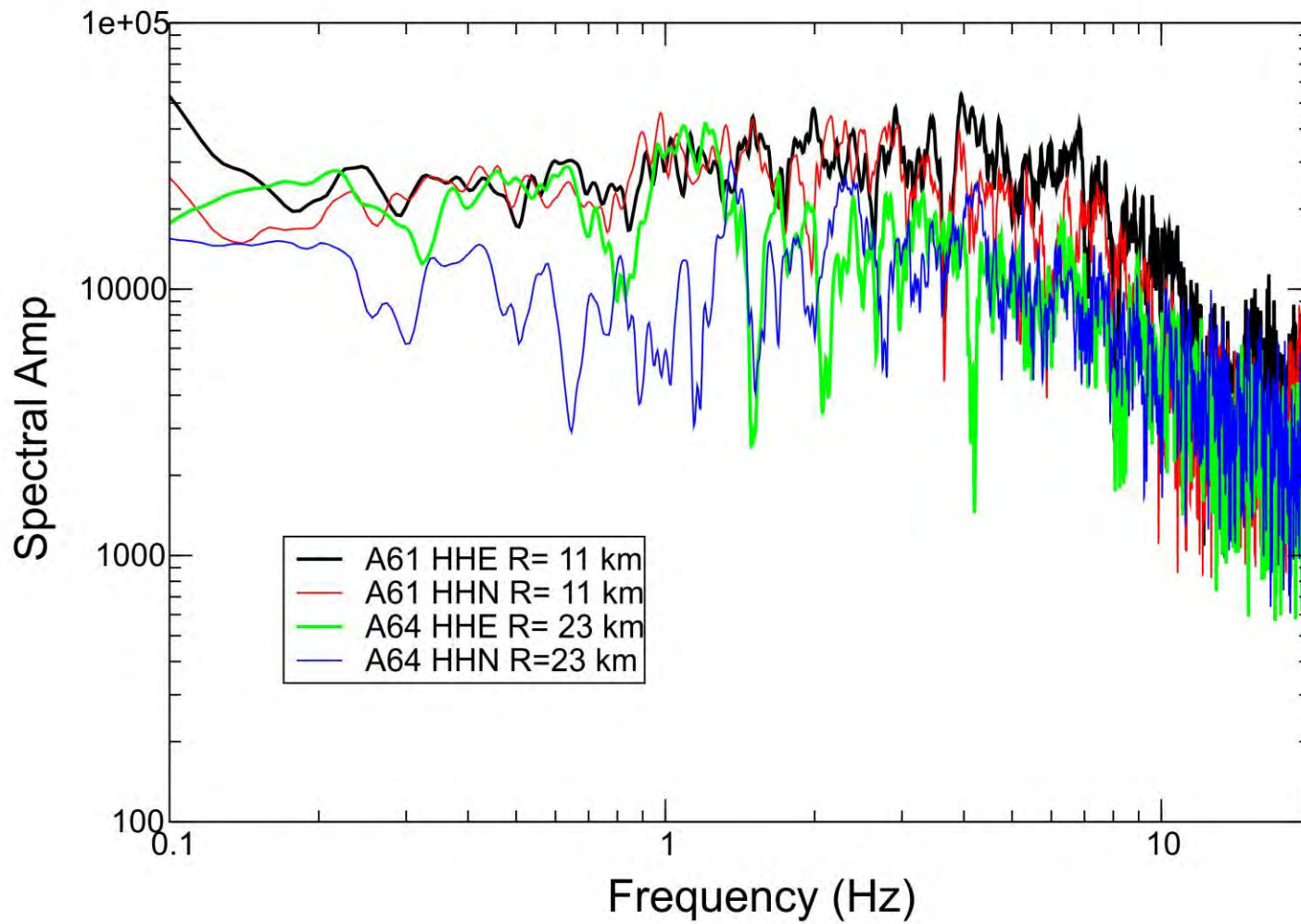
Comparing observed spectral amplitudes with those from reflectivity synthetics from plane-layered velocity model

- For Riviere du Loup earthquake, used finite source with rupture directivity (1.4 x 1.4 km)
- For 6/13/2003 earthquake, used point source
- Used slip velocity of 5.4 m/s, twice that used for WUS earthquake comparison with NGA east (Frankel, 2009), implying dynamic stress drop of 200 bars; 1 Hz not sensitive to this
- Focal mechanisms and seismic moments from Bob Herrmann

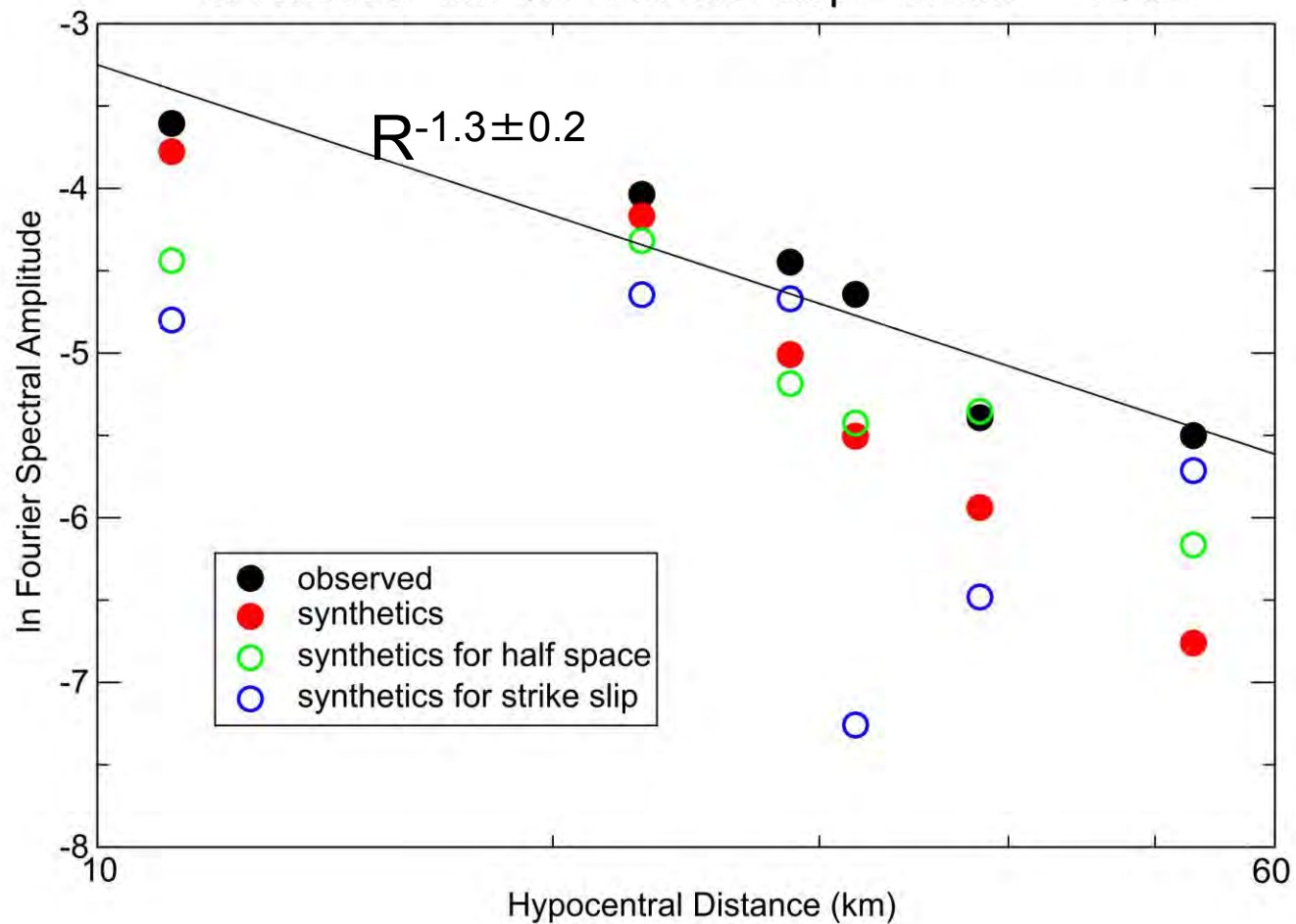
Riviere du Loup Earthquake 1 Hz



6/13/2003 M_n4.1 Displacement Spectra



6/13/2003 Mn 4.1 Mw 3.3 dep= 11 km 1 Hz



Conclusions

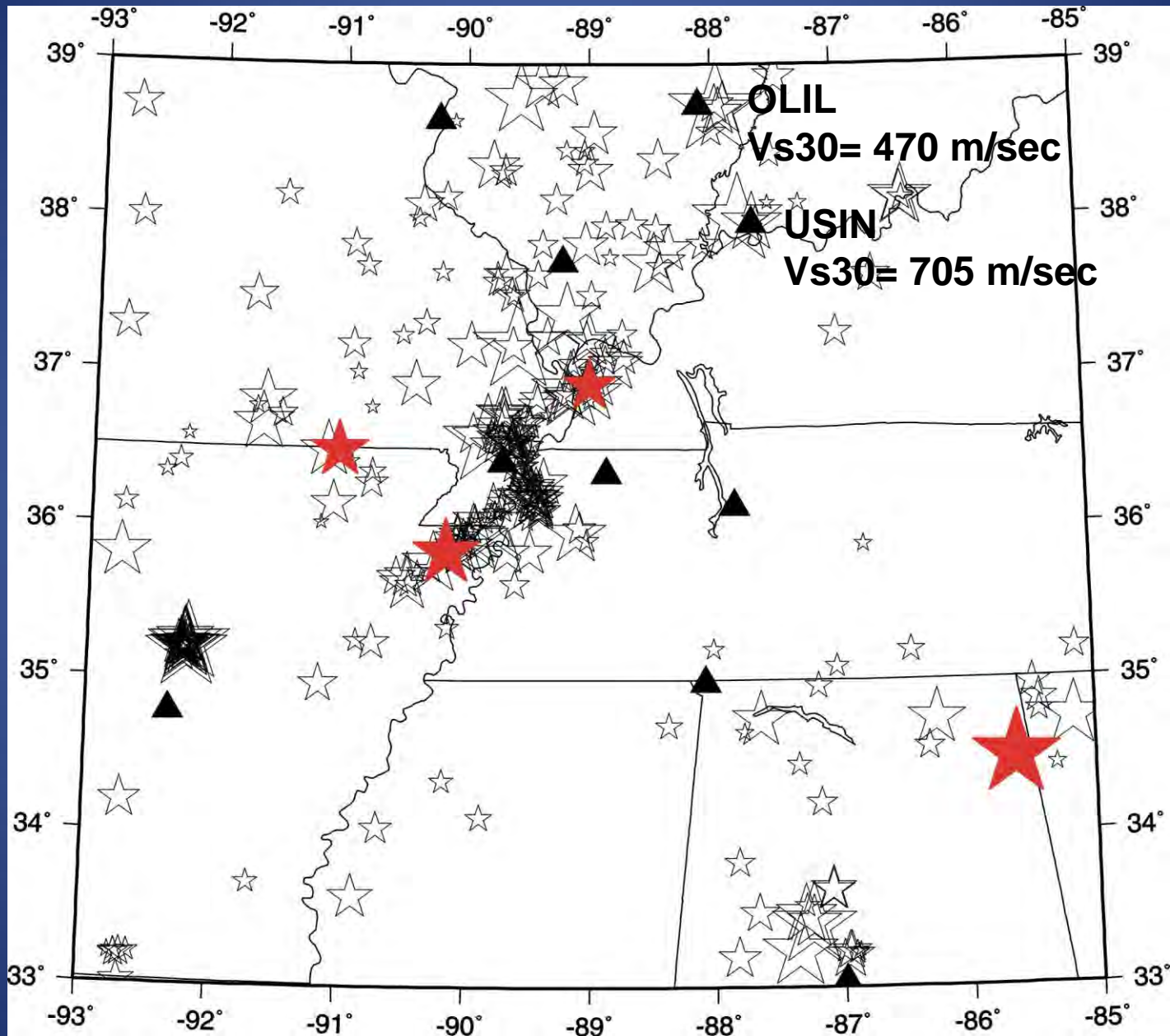
- Slower amplitude decay with distance of 14 Hz S-wave amplitude ($R^{-1.05}$) compared to 5 Hz ($R^{-1.35}$) and 1 Hz ($R^{-1.6}$). Apparent geometrical spreading depends on frequency
- $R^{-1.05}$ determined from 14 Hz data would be the steepest true geometrical spreading decay, since Q was not corrected for
- Based on results of synthetics, apparent geometrical spreading at 1 Hz is dependent on radiation pattern of source and, at least for Riviere du Loup earthquake, upward rupture directivity. Steep apparent geometrical spreading at 1 Hz is consistent with synthetics using radiation pattern and directivity

- Should not use frequency-dependent geometrical spreading and Brune spectral shape in stochastic simulations since close-in spectra do not have simple Brune shape
- Recommend use of R^{-1} geometrical spreading (dist < 70 km) based on high-frequency observations not contaminated by radiation pattern and directivity
- Apparent geometrical spreading at 1 Hz is dependent on rupture directivity and radiation pattern; better to use deterministic synthetics using plane layers for ≤ 1 Hz; should develop GMPE's for different focal mechanisms using various slip distributions and hypocenters on the rupture plane
- I am currently working on this procedure to make new ENA GMPE's using hybrid methodology for broadband synthetics (deterministic + stochastic) for finite faulting (Frankel, 2009)

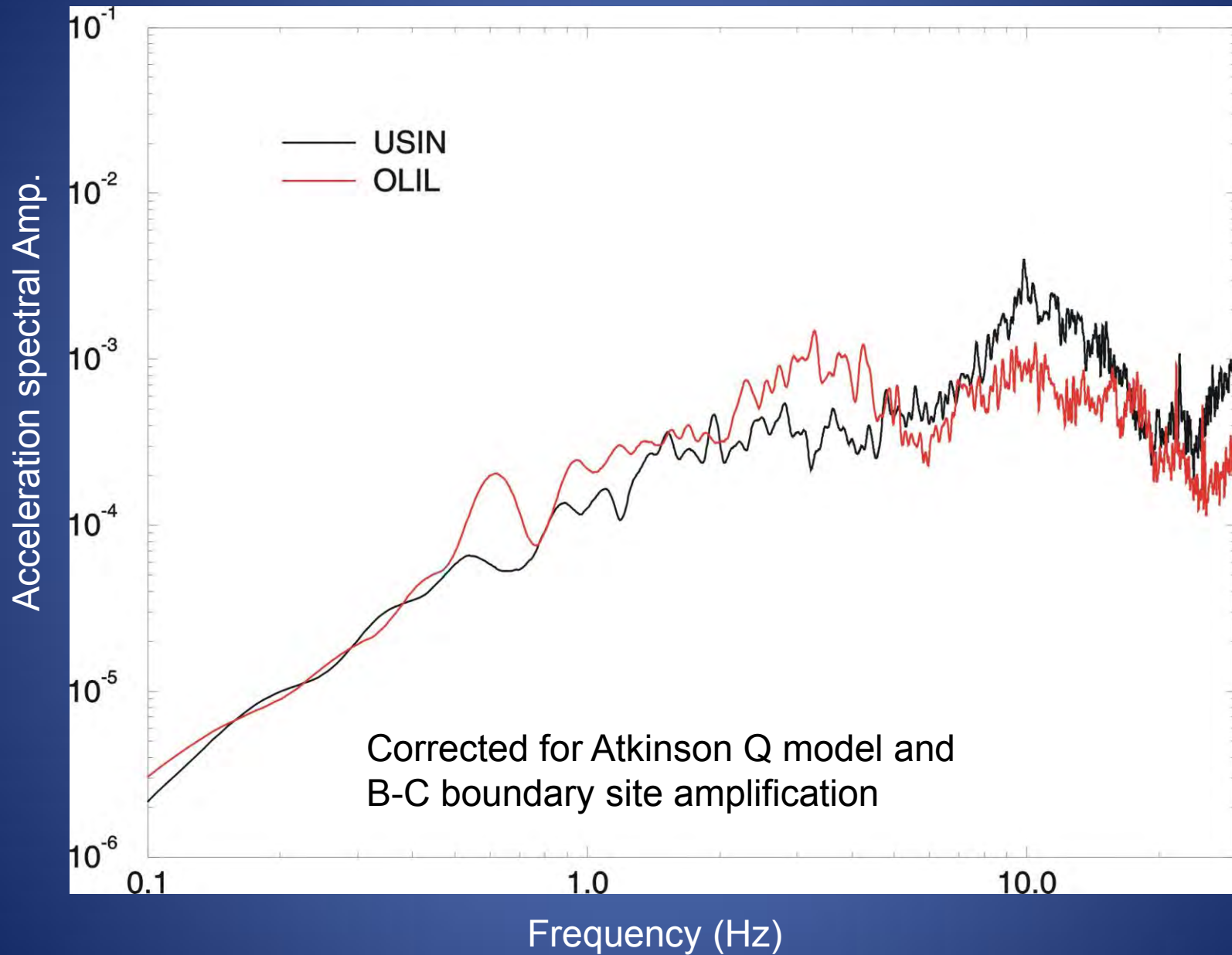
acknowledgments

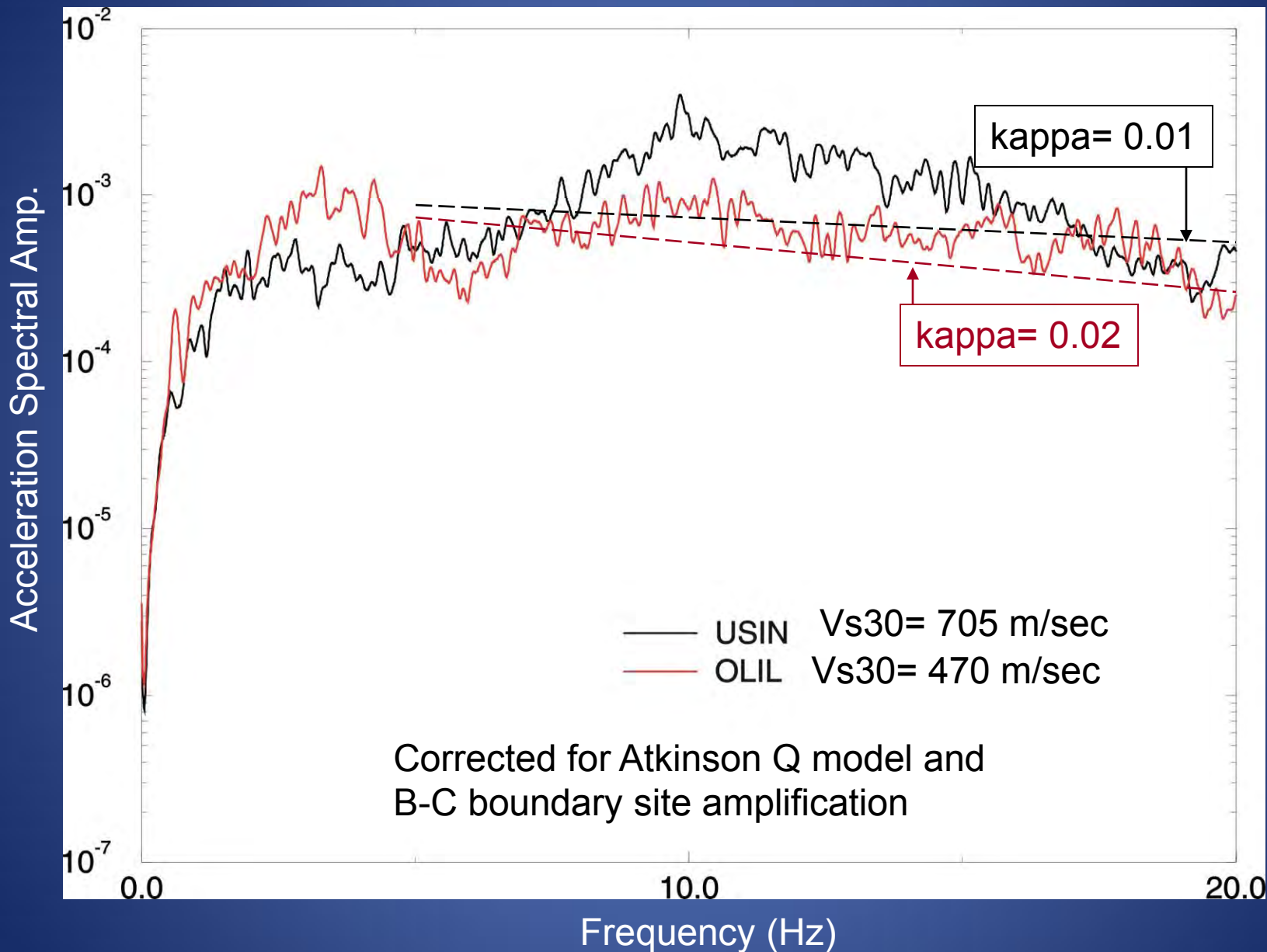
- Seismograms from Geological Survey of Canada; also used their hypocenters
- PEER- NGA East (Christine Goulet) supplied some of the data

What is kappa (high-frequency spectral falloff) for CEUS B-C sites? Vs30= 760 m/sec



5/1/05 earthquake, NE Arkansas, M4.2, $f_c = 2$ Hz (at OLIL)





We used kappa=0.01 for CEUS B-C sites

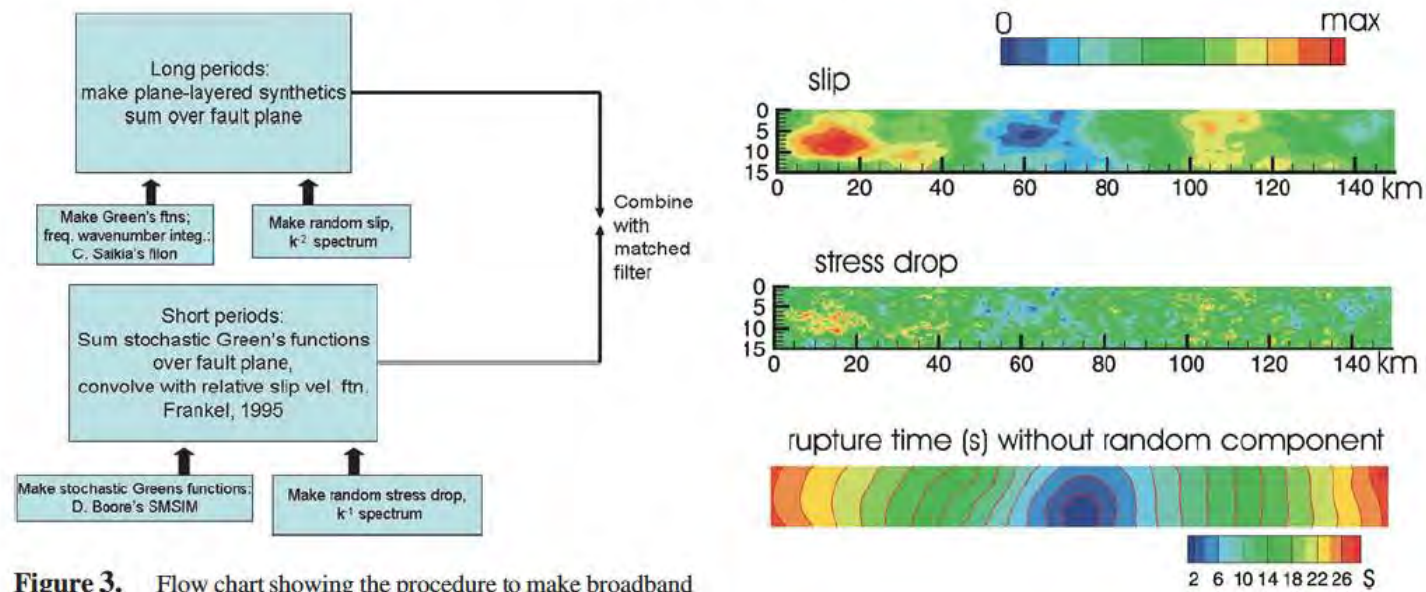


Figure 3. Flow chart showing the procedure to make broadband synthetic seismograms.

From Frankel (2009)

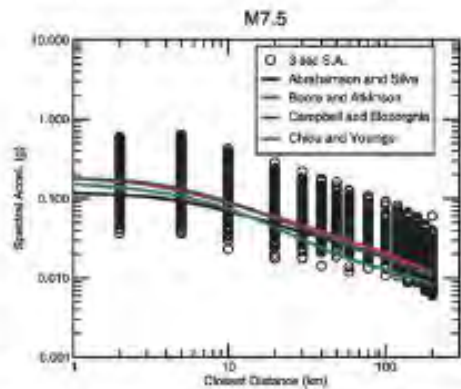
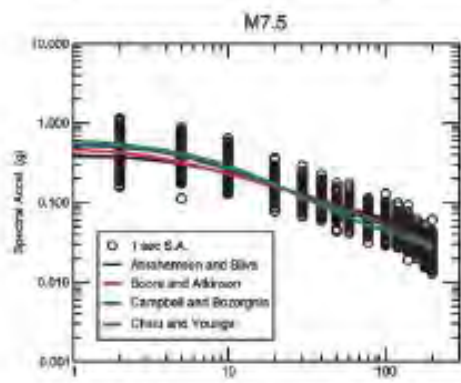
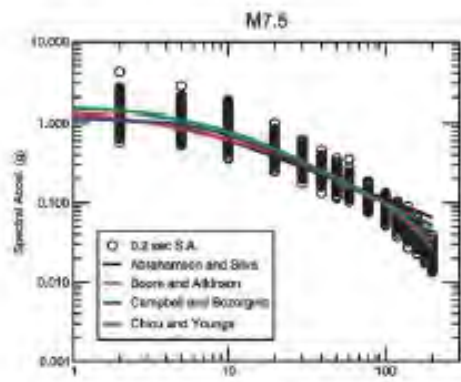


Figure 10. SAs (open circles) from the broadband synthetics of the nine simulations of $M 7.5$ earthquakes, for 0.2 (top panel), 1.0 (middle panel), and 3.0 sec periods (bottom panel). Solid lines are predictions of the median values from the NGA relations.

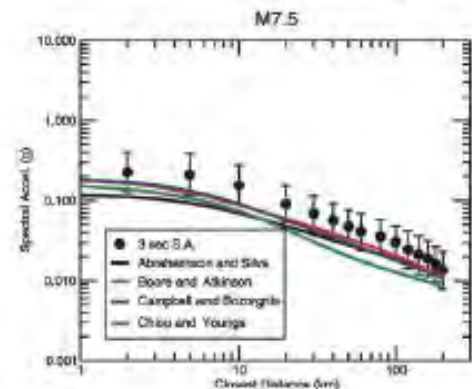
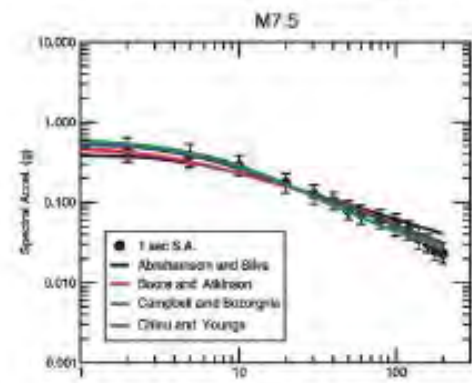
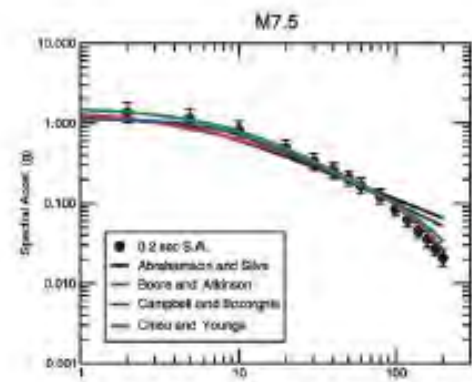


Figure 11. Median values of the SAs (solid circles with error bars for ± 1 standard deviation, based on the variation between the values at each distance) at each distance for 0.2 (top panel), 1.0 (middle panel), and 3.0 sec periods (bottom panel) from the broadband synthetics for $M 7.5$ compared to the predictions from the NGA relations.

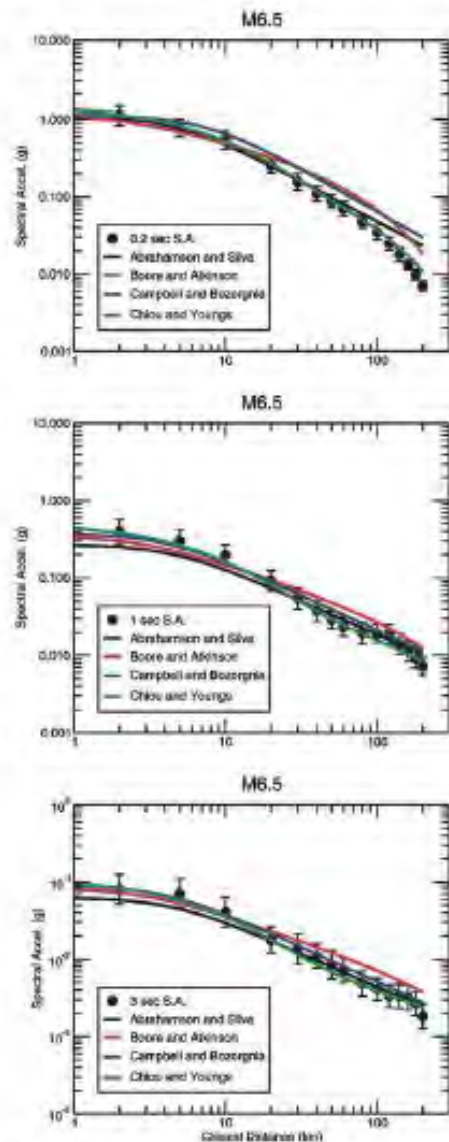


Figure 12. Median values of the SAs (solid circles with error bars for ± 1 standard deviation) at each distance for 0.2 (top panel), 1.0 (middle panel), and 3.0 sec periods (bottom panel) from the broadband synthetics for $M 6.5$ compared to the predictions from the NGA relations.

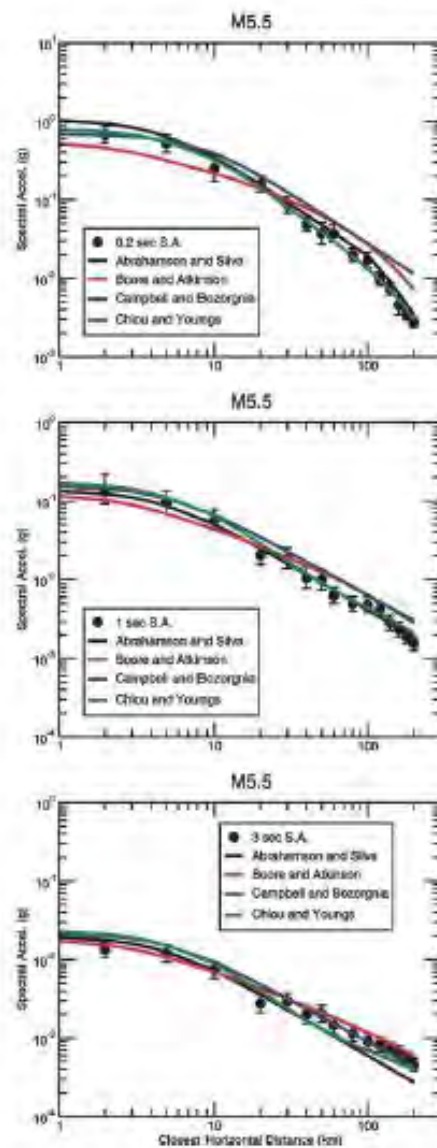


Figure 13. Median values of the SAs (solid circles with error bars for ± 1 standard deviation) at each distance for 0.2 (top panel), 1.0 (middle panel), and 3.0 sec periods (bottom panel) from the broadband synthetics for $M 5.5$ compared to the predictions from the NGA relations.

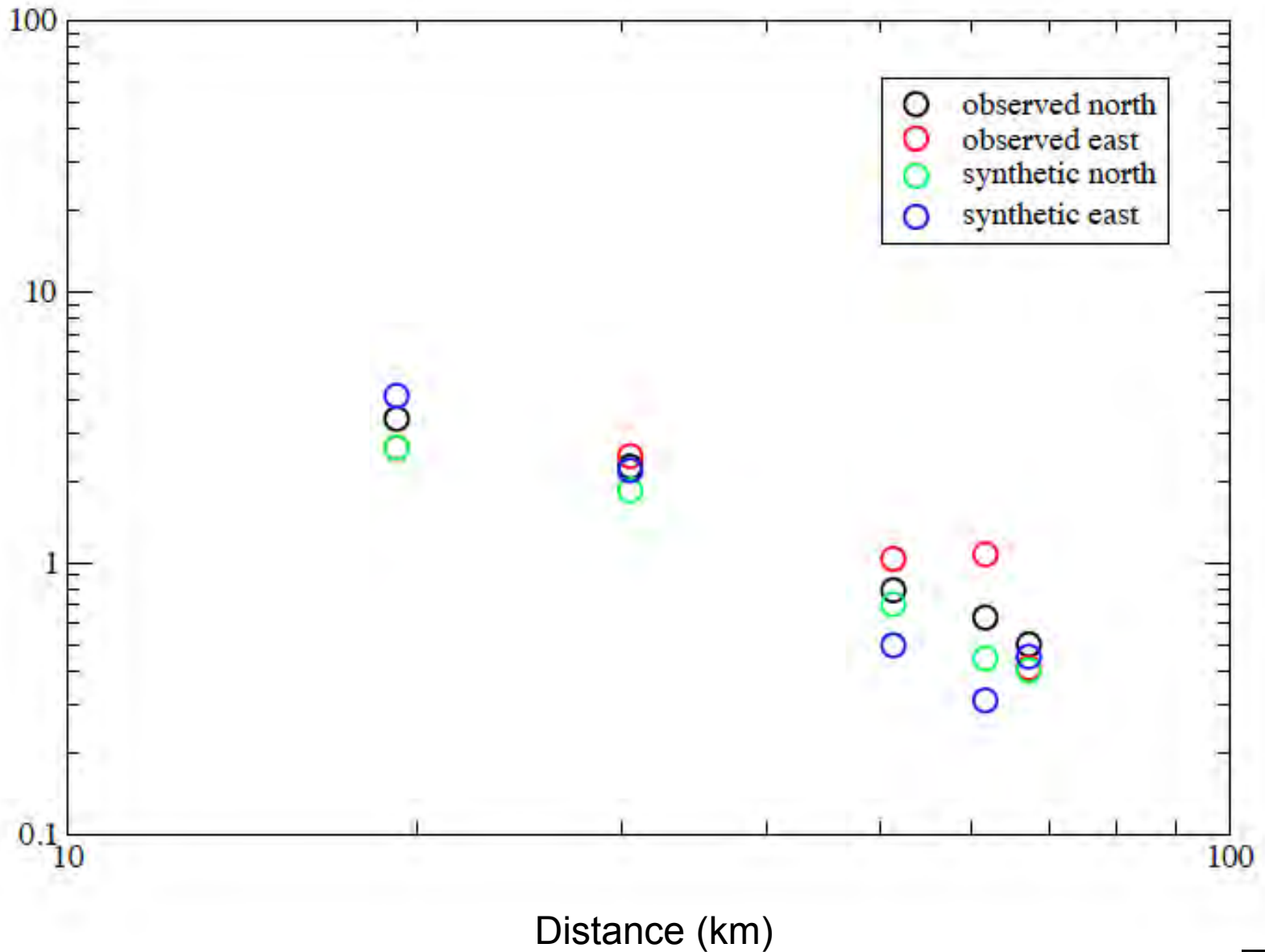
For Riviere du Loup earthquake, used stress drop of 200 bars (stochastic synthetics) and average slip velocity of 5.4 m/s (deterministic synthetics).

For Saguenay used 500 bar stress drop and 13.5 m/s slip velocity.

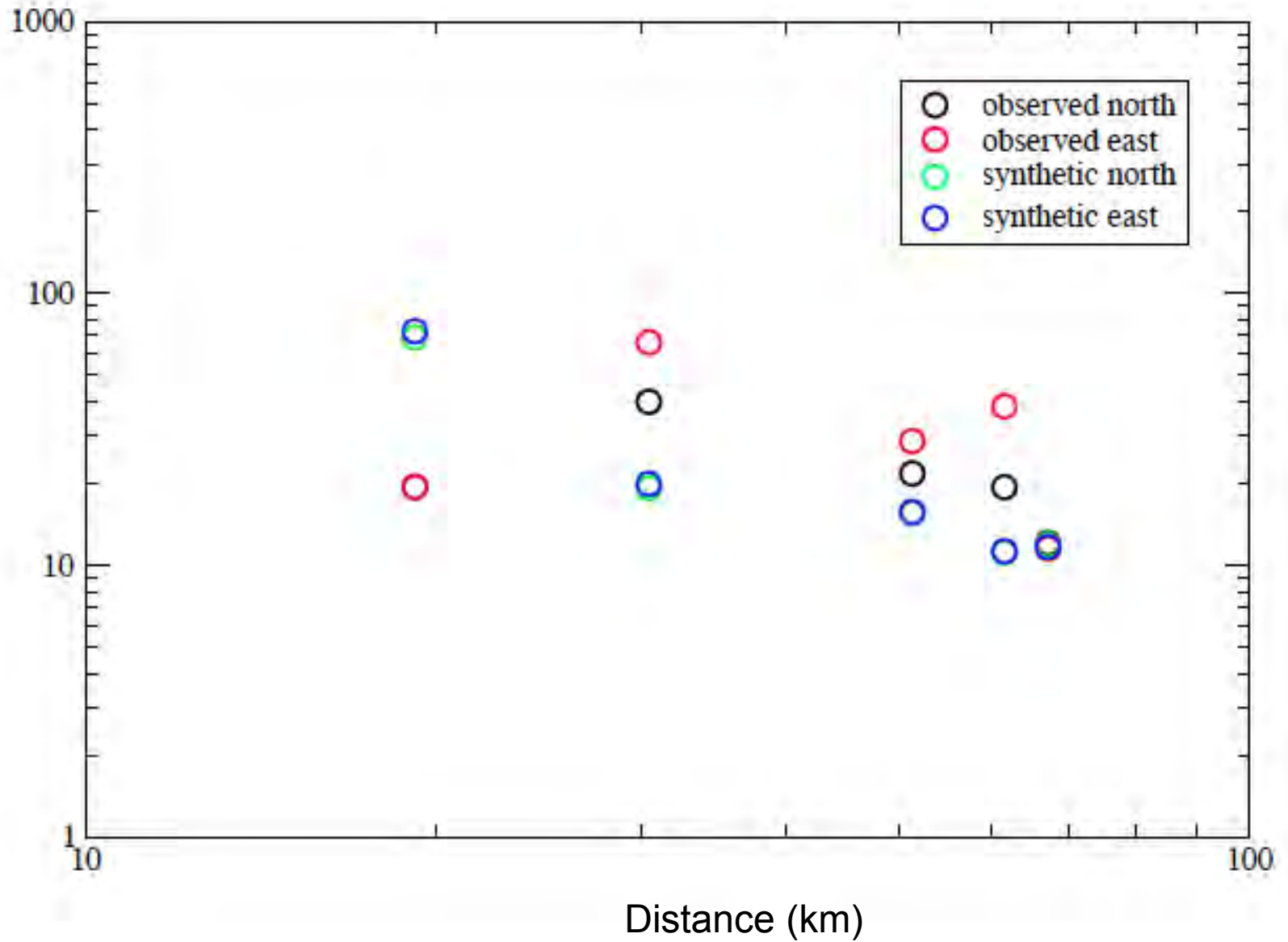
ENA crustal model from Hartzell and Mendoza and hard-rock site condition for stochastic synthetics

3 Hz crossover frequency between deterministic and stochastic synthetics

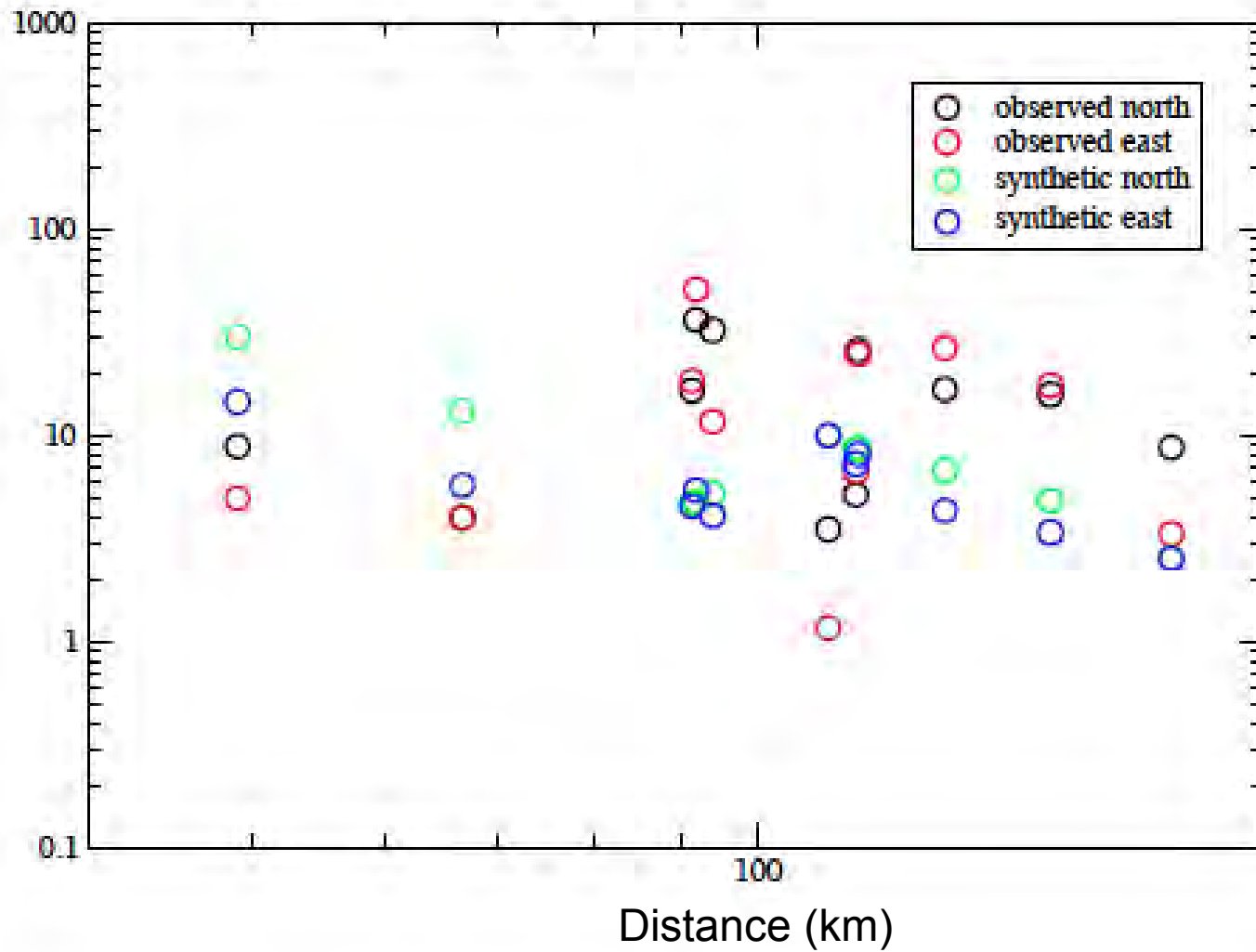
Riviere du Loup 1 Hz S.A.



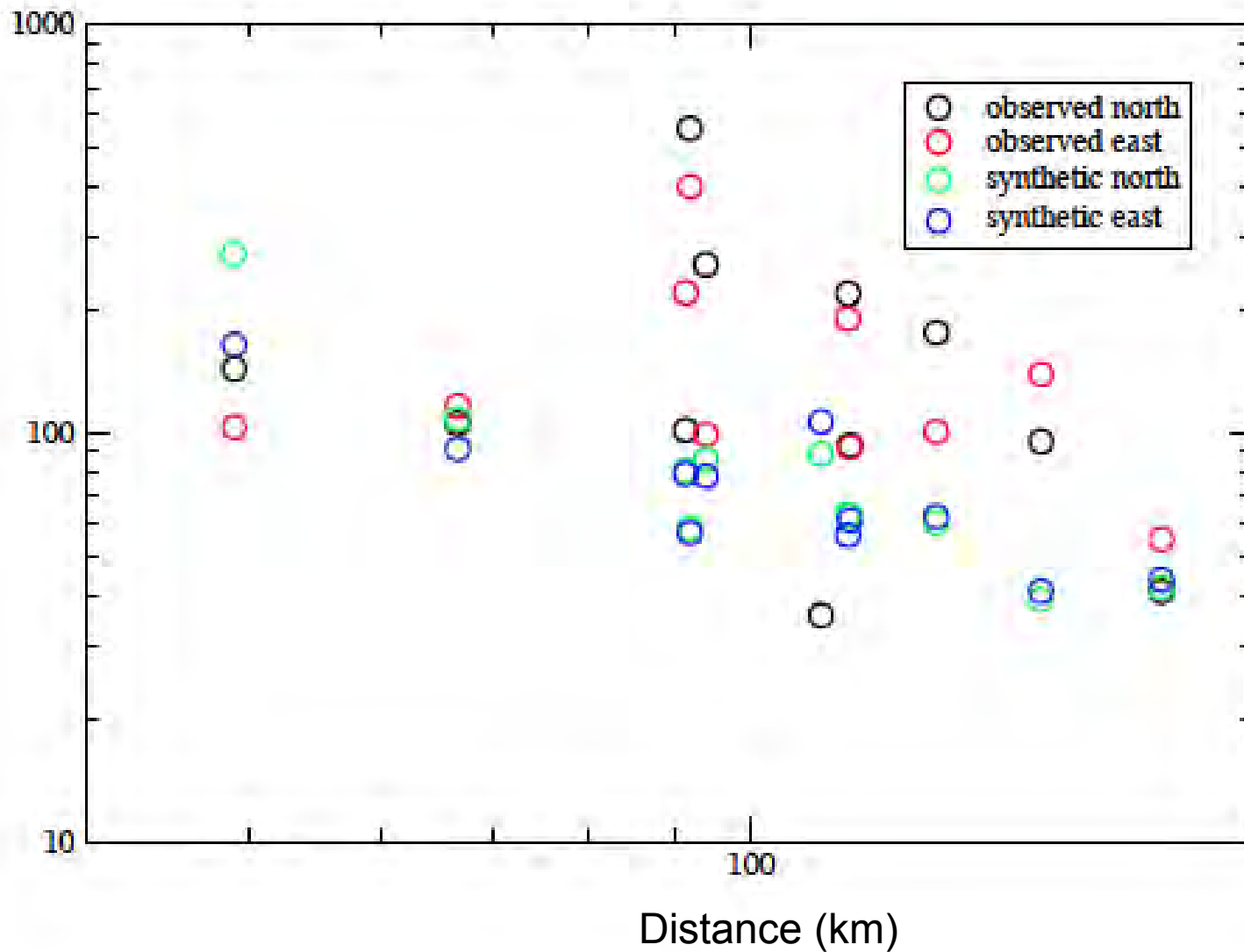
Riviere du Loup 5 Hz S.A.



Saguenay 1 Hz S.A.



Saguenay 5 Hz S.A.



S-wave amplitude:

$$A_S(f, R) = P_{\theta\phi} S(f) G(f) I(f) R^{-\gamma} e^{-\pi f t_s / Q_S}$$

coda-wave amplitude at lapse time t_E :

$$A_C(f, t_E) = P_{ave} S_{ave}(f) G(f) I(f) C(f) t_E^{-2} e^{-\pi f t_E / Q_C}$$

$$A_S(f, R) / A_C(f, t_E) = R^{-\gamma} e^{-\pi f t_s / Q_S} F(f, t_E) P_{\theta\phi} S(f) / P_{ave} S_{ave}(f)$$

P = radiation pattern

S = source spectrum

G = site amplification

I = instrument response

C = scattering coefficient